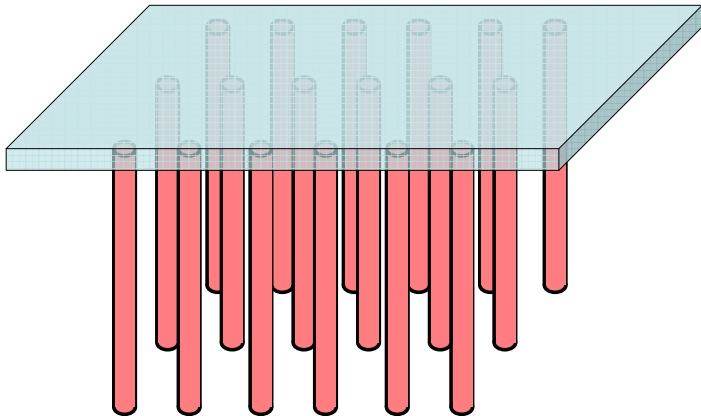


# Modeling large foundation rafts

**Andrzej Truty**  
**ZACE Services**

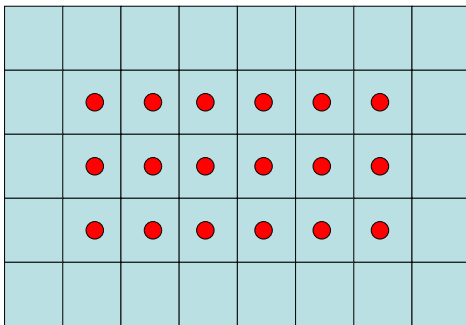
27.08.2008

# Problem to be solved



# Where is the problem ?

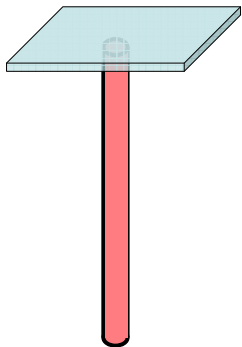
- If we have lot of piles it is almost impossible to
  - 1 Create 3D compatible FE mesh for plate-piles-interfaces system
  - 2 Compute the problem on a PC platform
  - 3 Each redesign of piles generates new complex 3D mesh



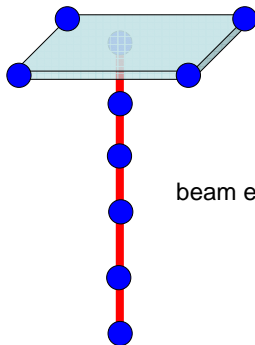
**Conclusion: we need absolutely a simplified treatment**

# Real vs FE model

plate-pile connection



Shell Q4

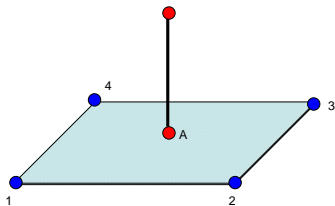


beam elements

# Requirements

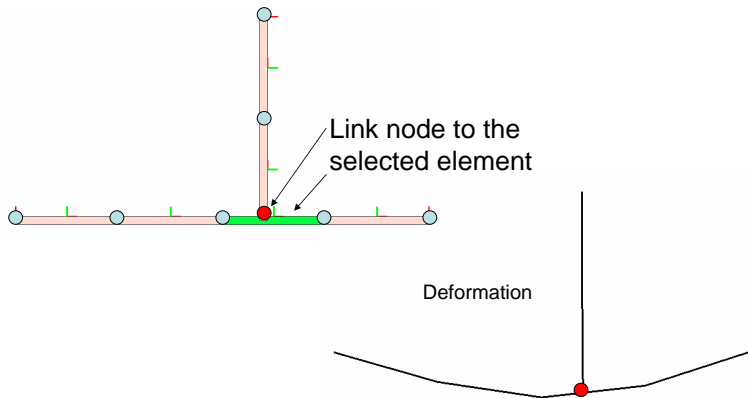
- Piles are modeled with aid of beam elements
- Beams are embedded in continuum without any restriction put on FE meshes
- Beam nodes can be connected to other elements like shells/beams/membranes/continuum not necessarily at element vertices
- Beam nodes can be connected to other elements via selected set of degrees of freedom
- The sliding interface between beam and continuum is created automatically
- The additional interface between bottom of the pile and subsoil can be optionally added
- Nodal forces can be applied at any point on the raft
- Penalty approach is not accepted (except for the frictional contact)

## New tools: Nodal link option

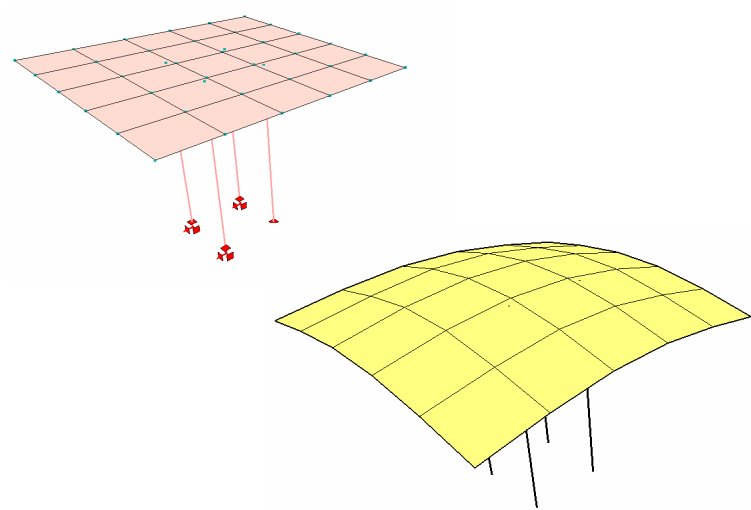


- Constraint equation(s):  $u_A = \sum_{i=1}^4 N_i u_i$
- Hence: stiffness, force vector from node A of a beam element is dispatched on shell degree of freedom
- DOF's of node A are dependent on other DOF's
- **Attention: constraints cannot be nested (!)**

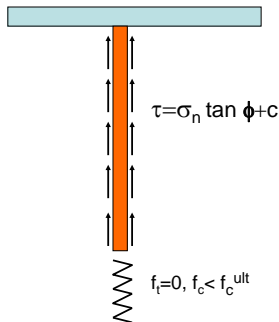
# Nodal link: example of beam-beam connection



# Nodal link: example of beam-shell connection



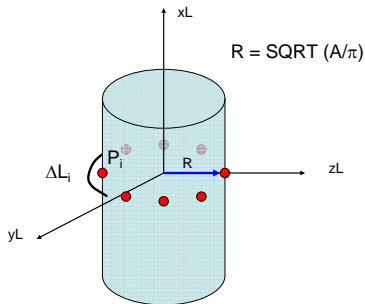




How to estimate  $\sigma_n$  ?

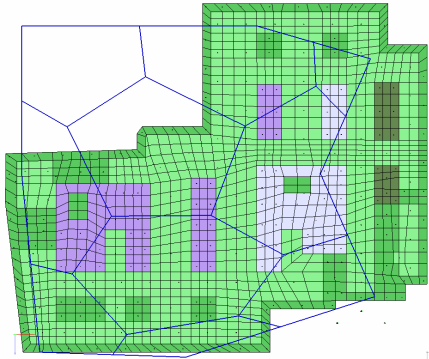
NB. We can leave  $\phi = 0$  and make contact purely adhesive like in codes for pile design

# Sliding interface: $\sigma_n$ estimation



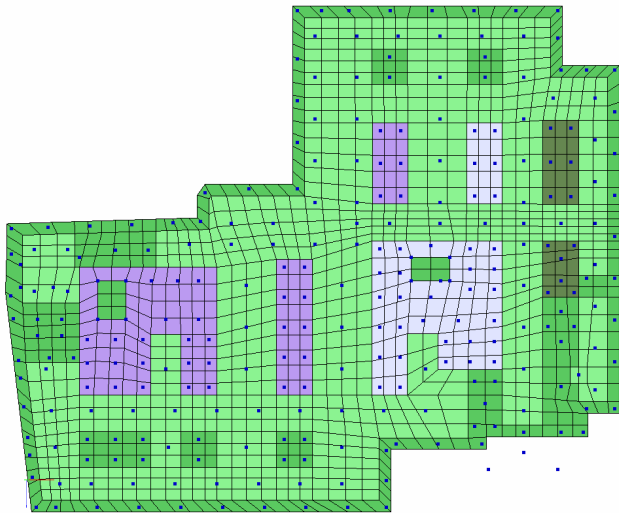
- $$\sigma_n = \frac{\int_L \min(\sigma_{ni}, 0) dl}{\int_L dl}$$
- $\sigma_{ni}$  is computed by effective stress transformation from the continuum elements in which interface and beam is embedded

# Practical example

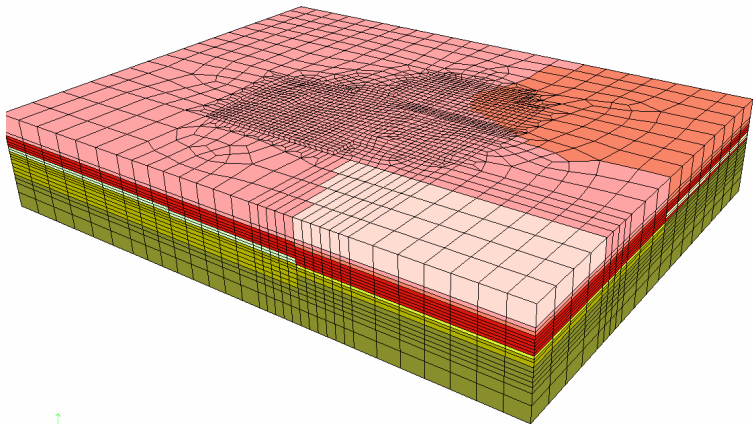


Goal: Estimate settlements using MC and HS-small models

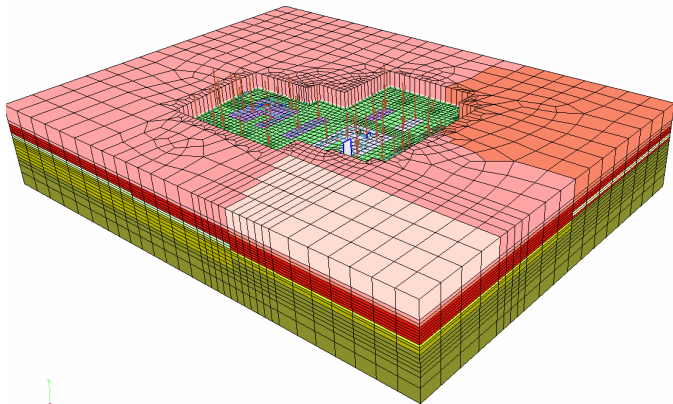
# Practical example: positioning of CFA piles



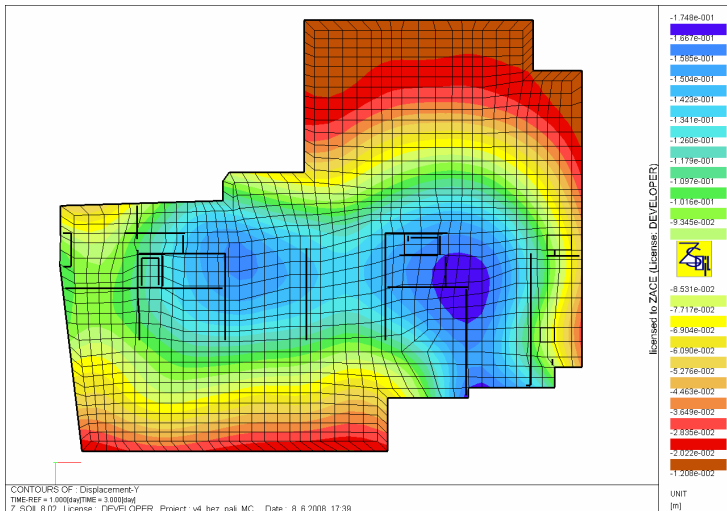
# Practical example: FE mesh



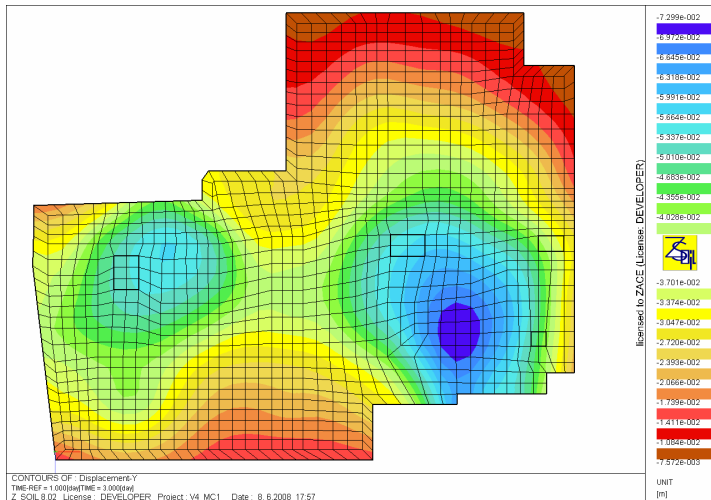
# Practical example: loading



# Results: MC model without piles ( $u_{max} = 17.5\text{cm}$ )

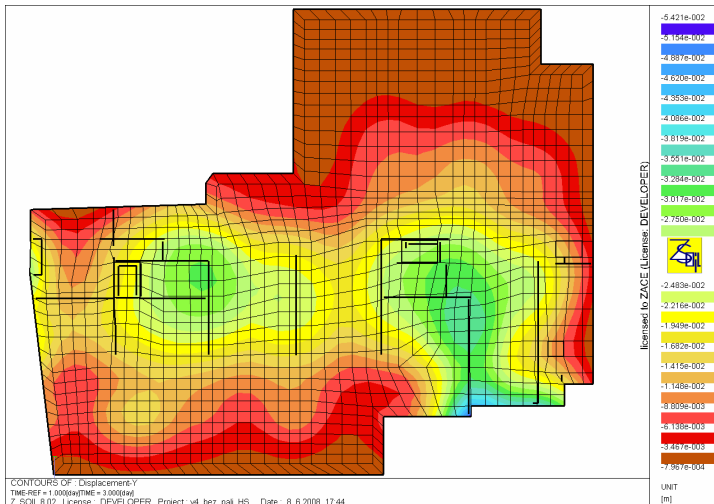


# Results: MC model with CFA piles ( $u_{max} = 7.3\text{cm}$ )

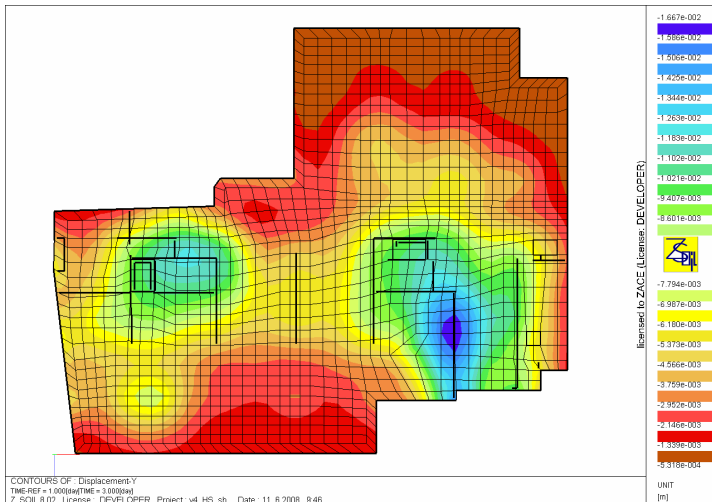




# Results: HS-small model without piles ( $u_{max} = 5.4\text{cm}$ )



# Results: HS-small model with piles ( $u_{max} = 1.7\text{cm}$ )



- This option allows to compute large foundation rafts
- It can be used also for nailing applications
- Redesign of piling is very fast as its discretization is disconnected from subsoil mesh
- This option allows to compute complicated tasks with PC resources