

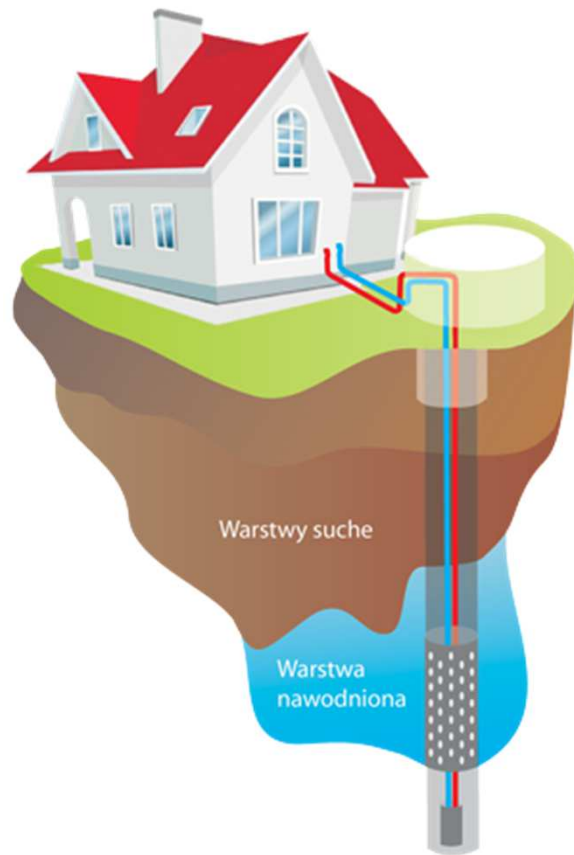
*ZSoil Days '2016*

Aleksander Urbański

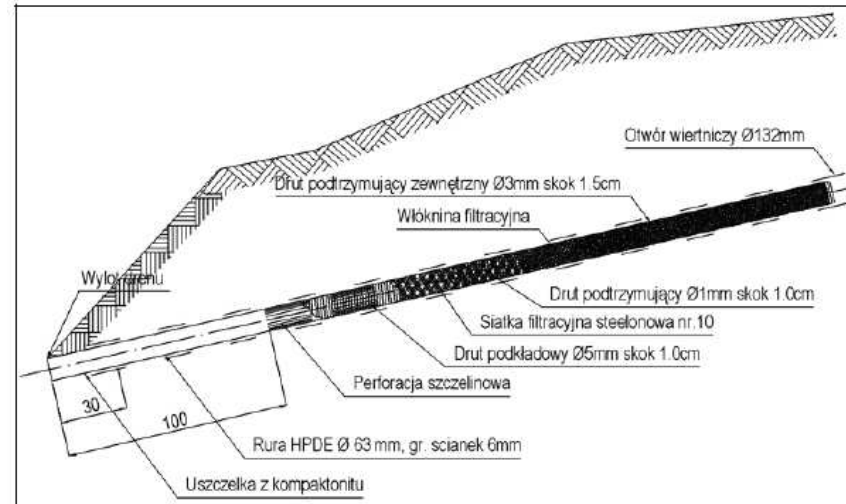
**Multi-scale analysis of a  
flow to drainage tubes**

# Application area

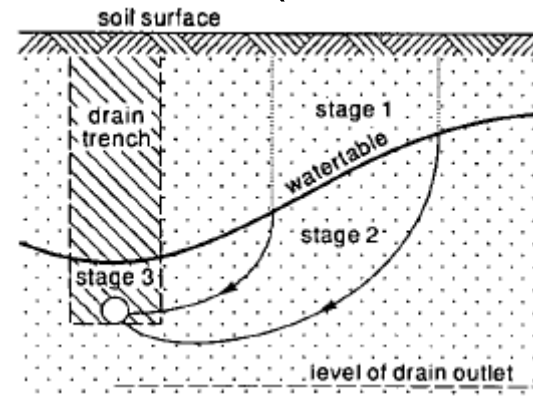
**drilled well (water supply)**



**drilled drain (slope stabilization)**



**French drain (dewatering)**

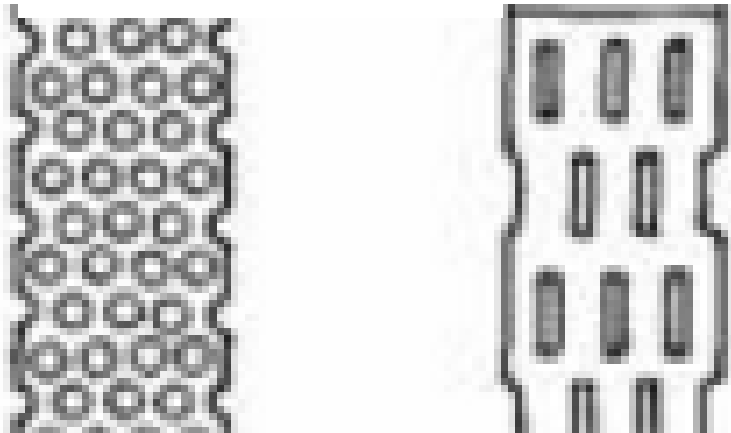


# Common feature



diameter  $D \sim 0.1$  m  
perforation of the pipe in mm

determine outflow  $q$



which results in filtration flow field  
(pressure  $p$ , flow  $q$ )  
in the area  $\sim 10$ m

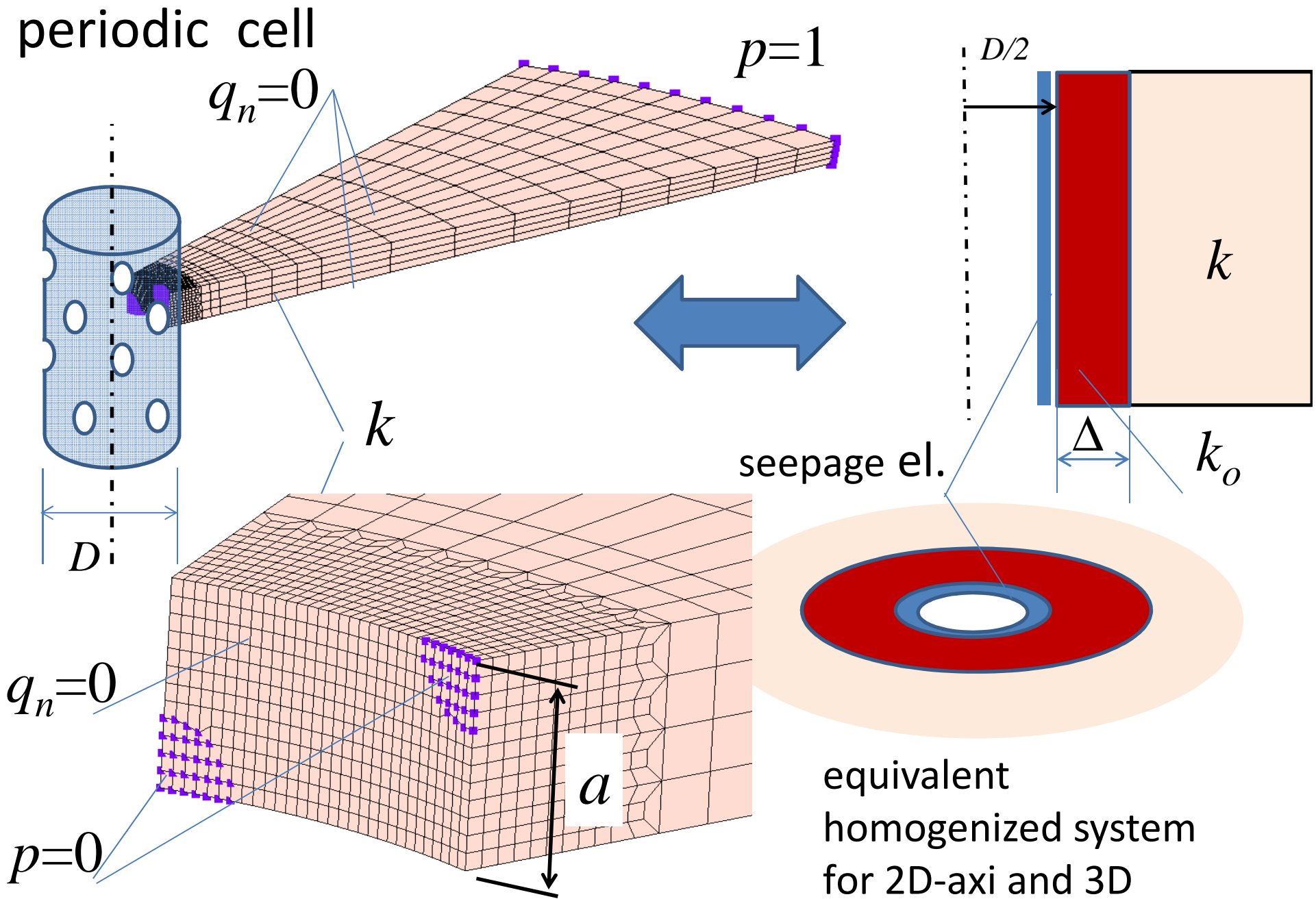
It is **difficult** to build **single model** dealing with filtration nearby drain tube (scale mm) and in the distance from it (m).

Scale separation leads to **multi-scale** problem

**micro** – 3D periodic cell in surrounding of the drain

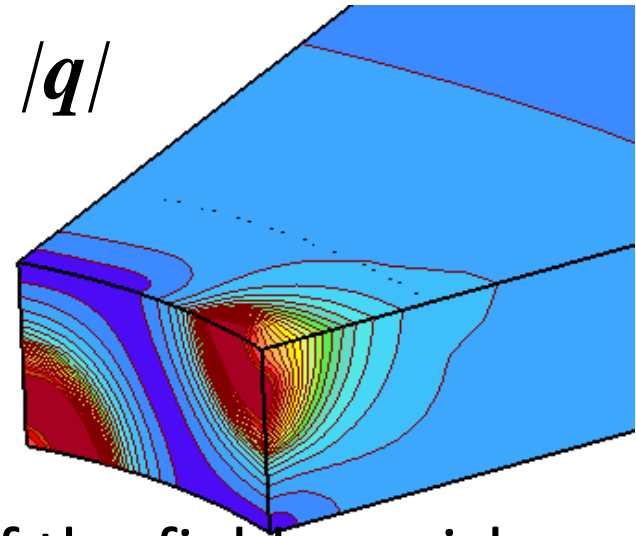
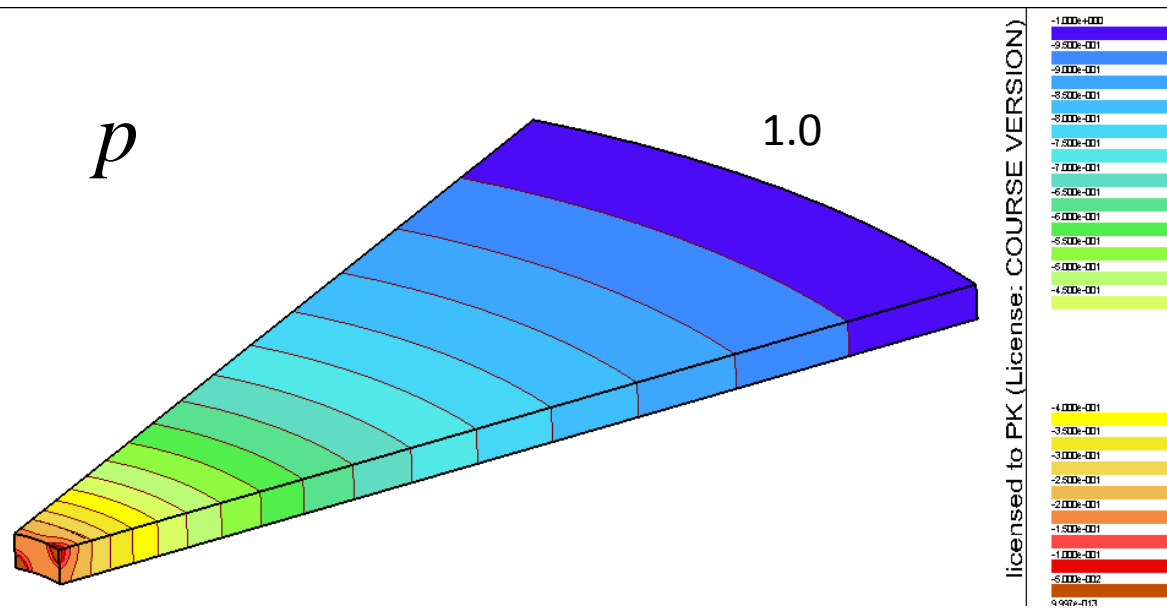
**macro** – whole system (2D or 3D)

# Numerical analysis basing on homogenization of the flow

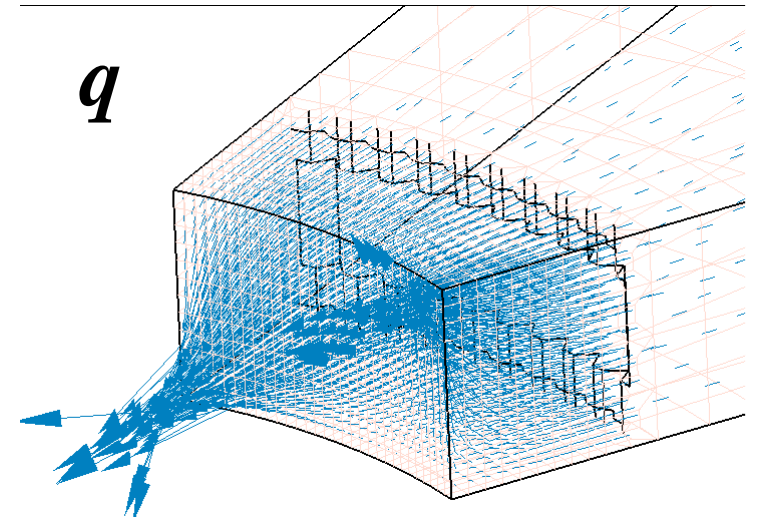
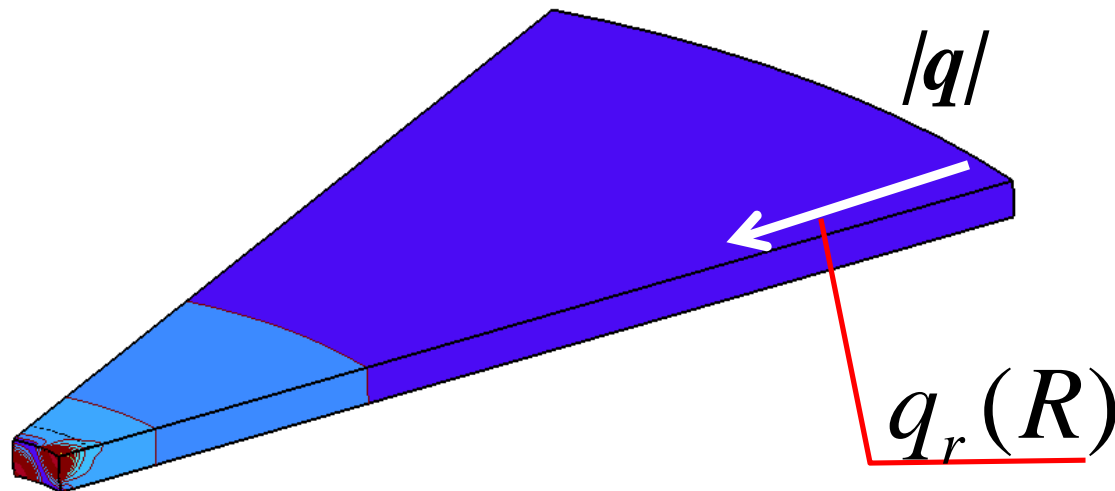


# Results on periodic cell

skipped gravity term  
in Darcy law



radius  $R$  set up such that fluctuations of the fields vanishes

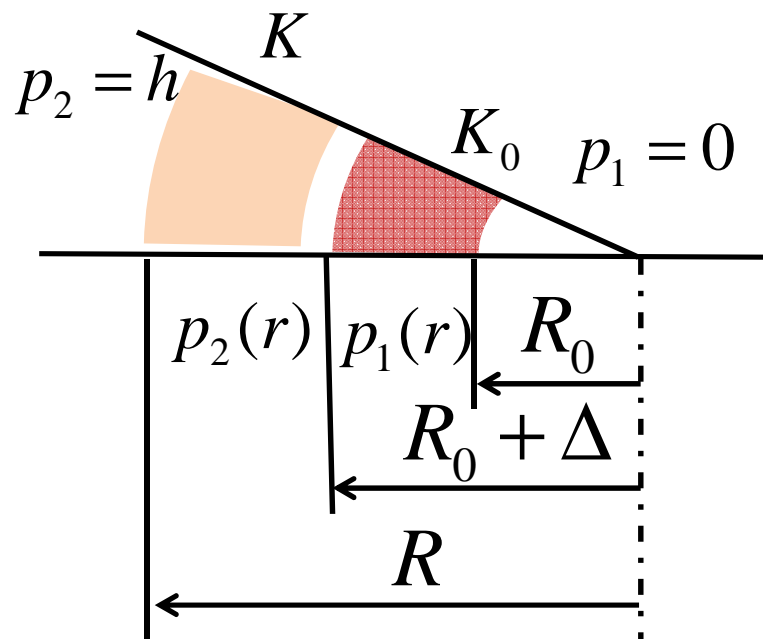


# Procedure to find properties of equivalent system

Assumed: axial symmetry, z-indepent:  $\frac{\partial p}{\partial \theta} = 0, \frac{\partial p}{\partial z} = 0, p = \frac{\hat{p}}{\gamma_F} [m]$   
 gravity potential = 0

$$\nabla^2 p = \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial p}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 p}{\partial \theta^2} + \frac{\partial^2 p}{\partial z^2} = \frac{\partial^2 p}{\partial r^2} + \frac{1}{r} \frac{\partial p}{\partial r} + \frac{1}{r^2} \frac{\partial^2 p}{\partial \theta^2} + \frac{\partial^2 p}{\partial z^2} = 0$$

$$\Rightarrow \frac{d^2 p}{dr^2} + \frac{1}{r} \frac{dp}{dr} = 0 \Rightarrow p(r) = C \ln|r| + D$$



boundary conditions:  $p_1(R_0) = 0$   
 $p_2(R) = h$

compatibility of:

flow  $K_0 \frac{\partial p_1}{\partial r} \Big|_{r=R_0+\Delta} = K \frac{\partial p_2}{\partial r} \Big|_{r=R_0+\Delta}$

pressures  $p_1(R_0 + \Delta) = p_2(R_0 + \Delta)$

\*

3D analysis of flow through

periodic cell:  $q_2(R)$  

$$Q = a \cdot 2\pi R \cdot q_2(R)$$

from the analytical  
solution of \*

$$Q = \frac{2\pi ahK_0}{\frac{K_0}{K} \ln \frac{R}{R_0 + \Delta} - \ln \frac{R_0 + \Delta}{R_0}}$$

then, for given  $q, K, R, R_0, h$  and assumed  $\Delta$

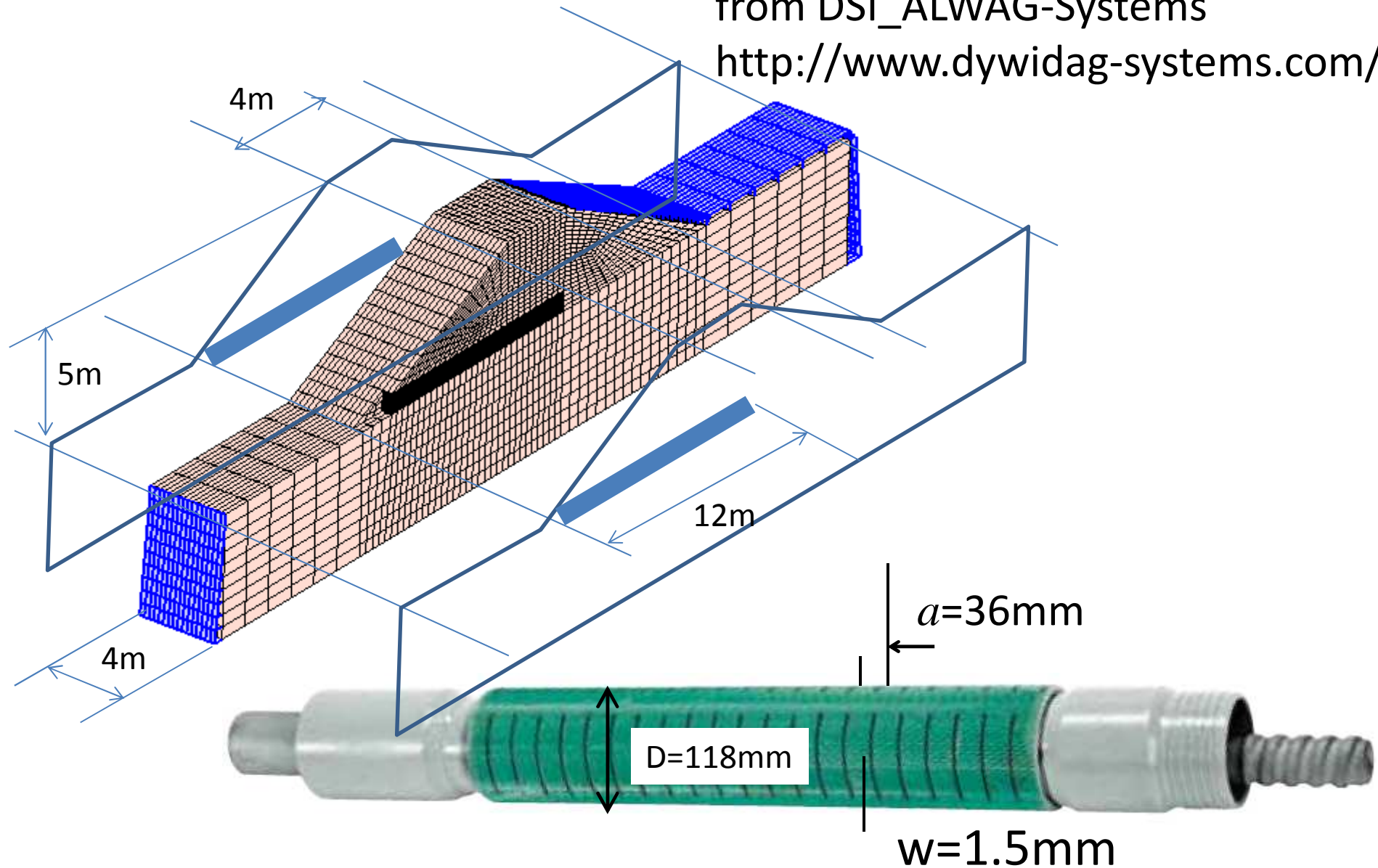
permeability of  
homogenized zone:

$$K_0 = \frac{\beta \ln \frac{R_0 + \Delta}{R_0}}{1 - \beta \ln \frac{R}{R_0 + \Delta}} K, \quad \beta = \frac{qR}{Kh}$$

# Application 1: **Drilled drain** in an earth dam

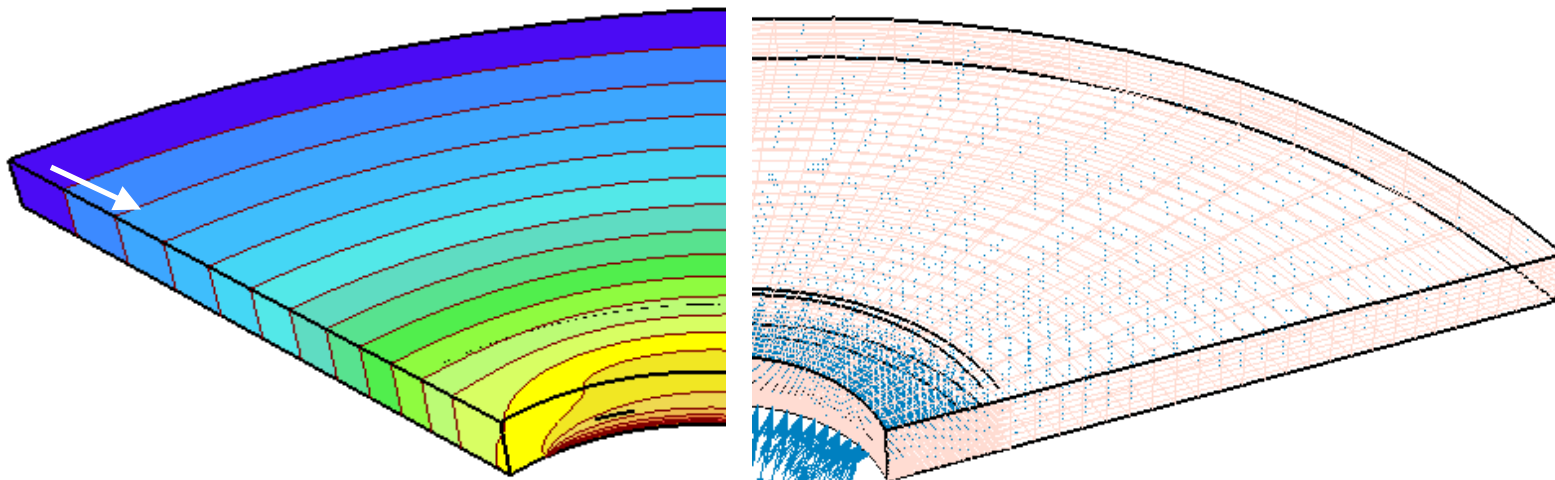
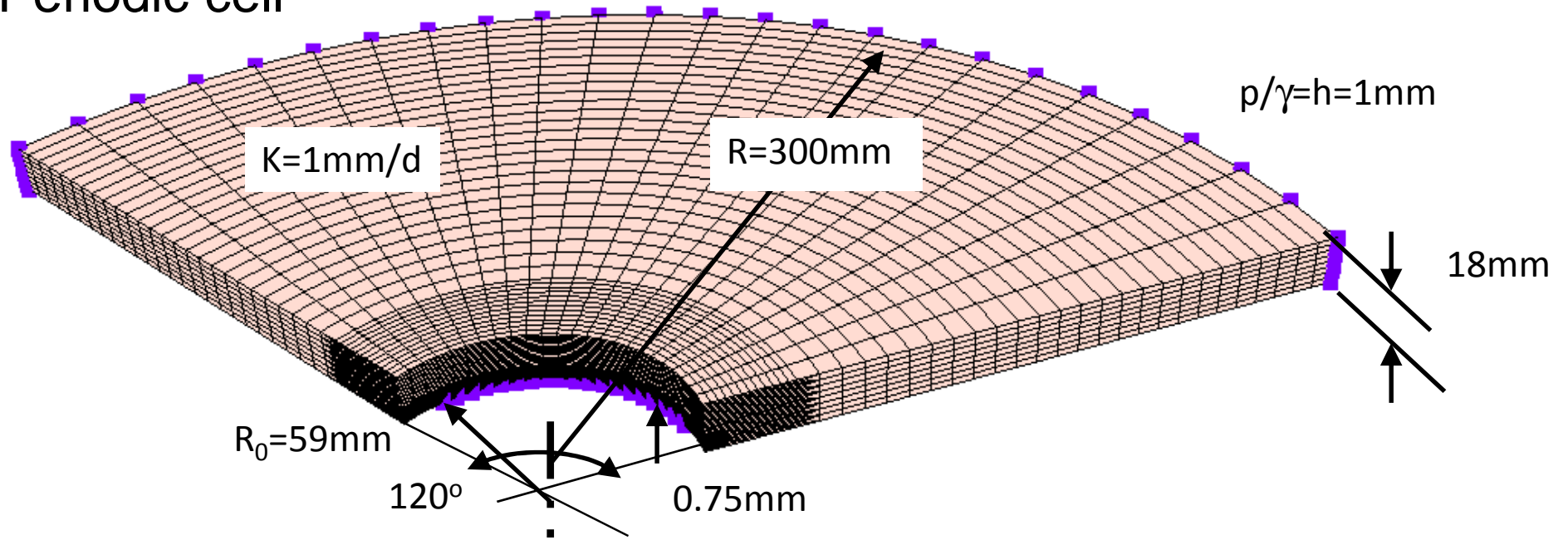
example: AT - Drainage System  
from DSI\_ALWAG-Systems

<http://www.dywidag-systems.com/>



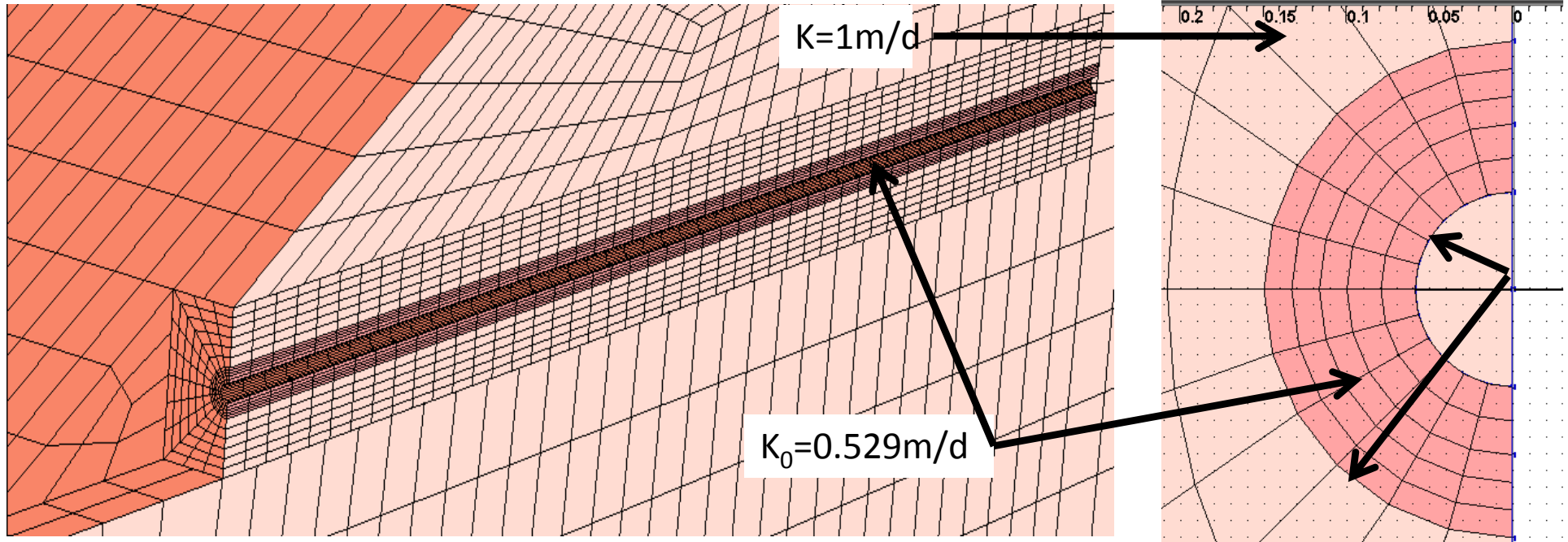


# Periodic cell



$$q(R=0.295) = 1.46 \cdot e^{-6} \left[ \frac{m}{d} \right] \Rightarrow \beta = \frac{qR}{Kh} = \frac{1.46e^{-6} \cdot 0.295}{1e^{-3} \cdot 1e^{-3}} = 0.407[-]$$

# 3D model of the drain

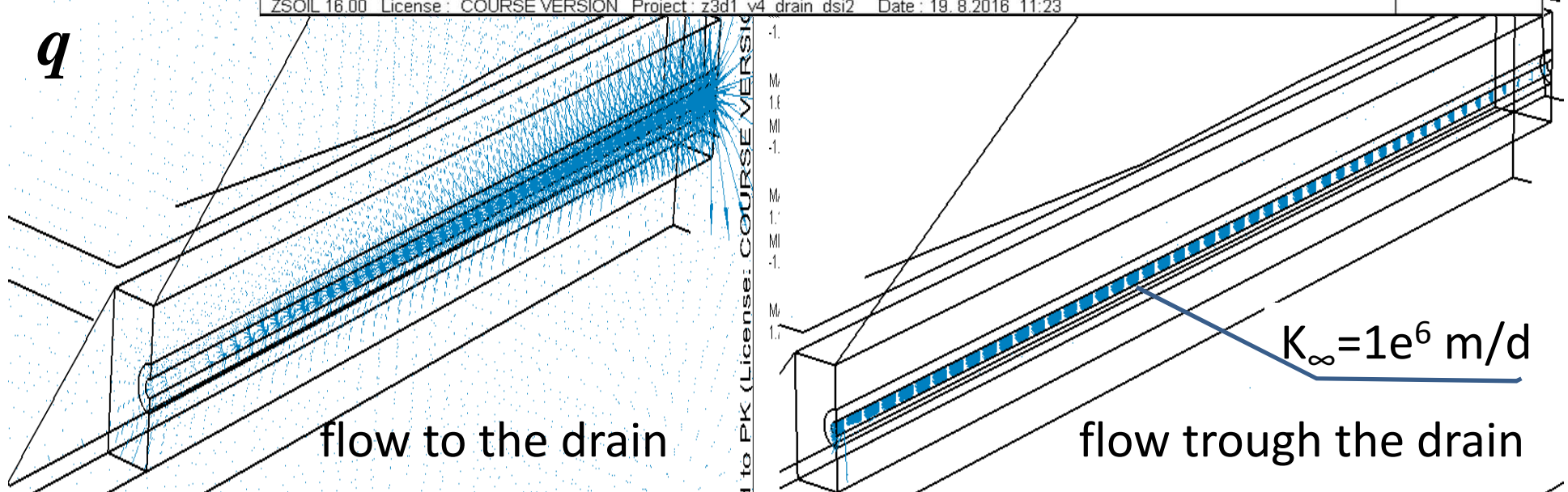
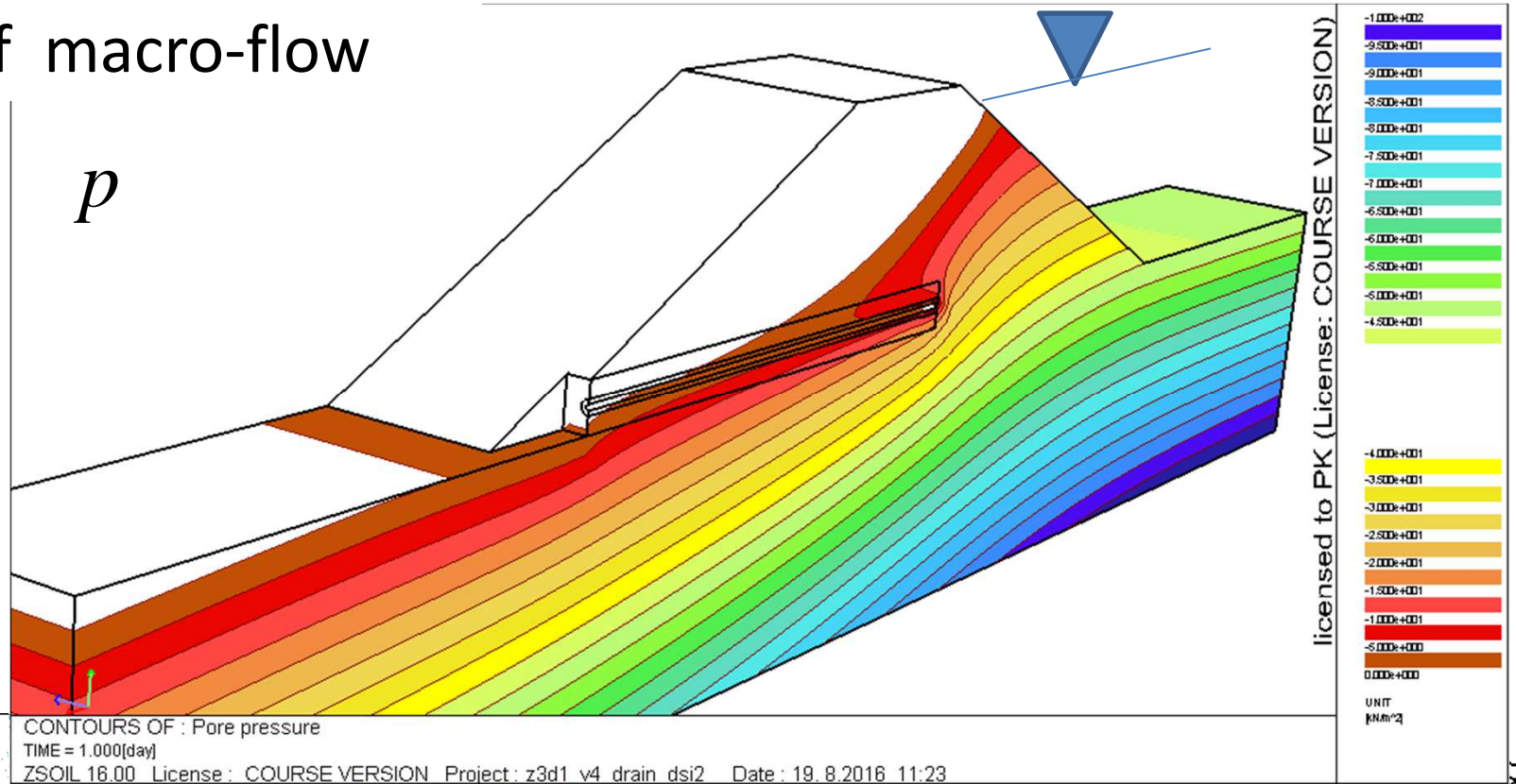


permeability of  
homogenized zone:

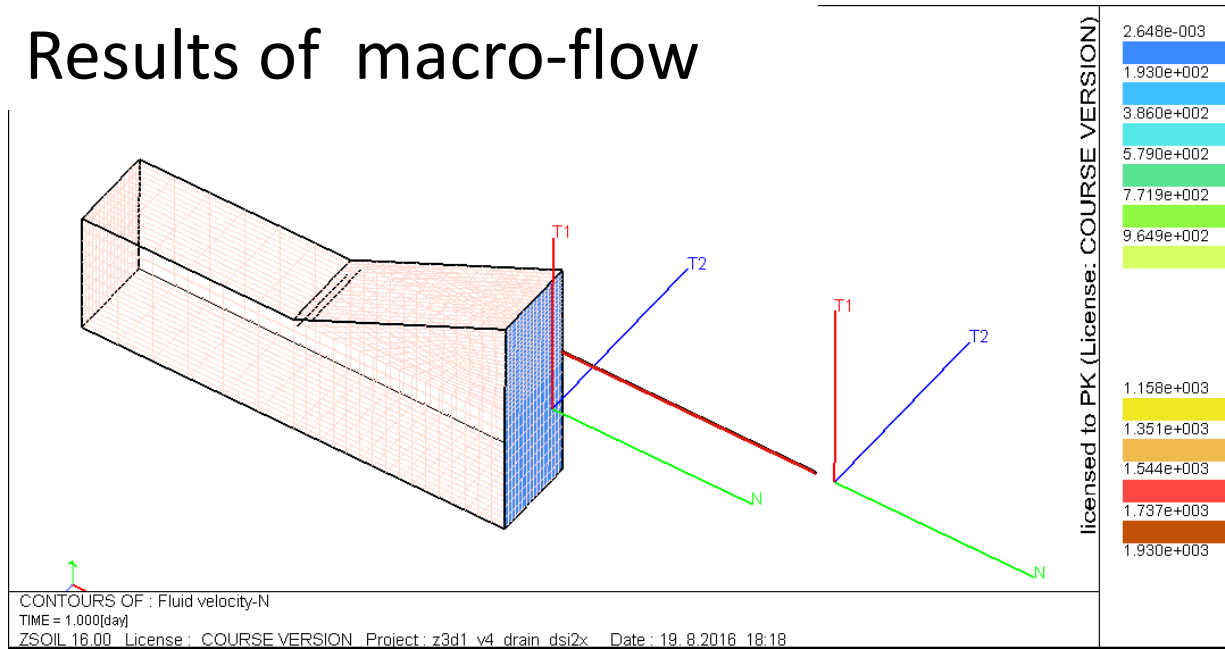
$$\beta = \frac{qR}{Kh} = 0.407[-], \quad R = 0.30m$$

$$K_0 = \frac{\beta \ln \frac{R_0 + \Delta}{R_0}}{1 - \beta \ln \frac{R}{R_0 + \Delta}} K = \frac{0.407 \ln 2.542}{1 - 0.407 \ln 2} K = 0.529 K,$$

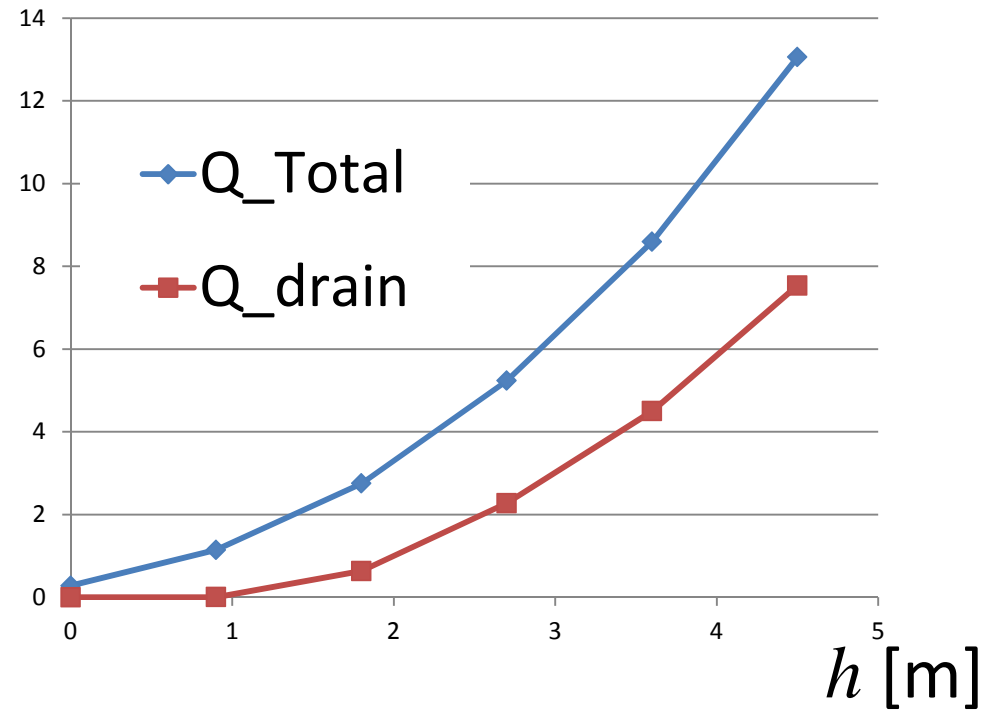
# Results of macro-flow



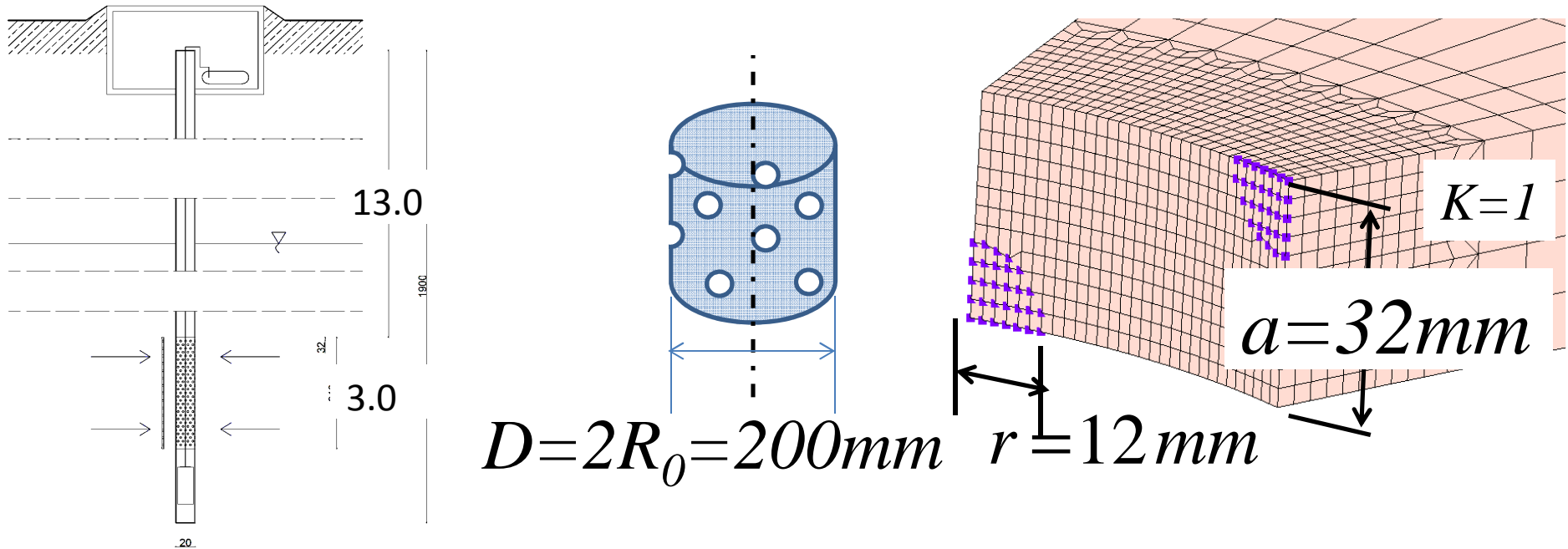
# Results of macro-flow



$Q$  [ $\text{m}^3/\text{d}$ ]



# Application 2: **Drilled well** in co-operation with phd. students: Karolina Kuc & Barbara Wilk



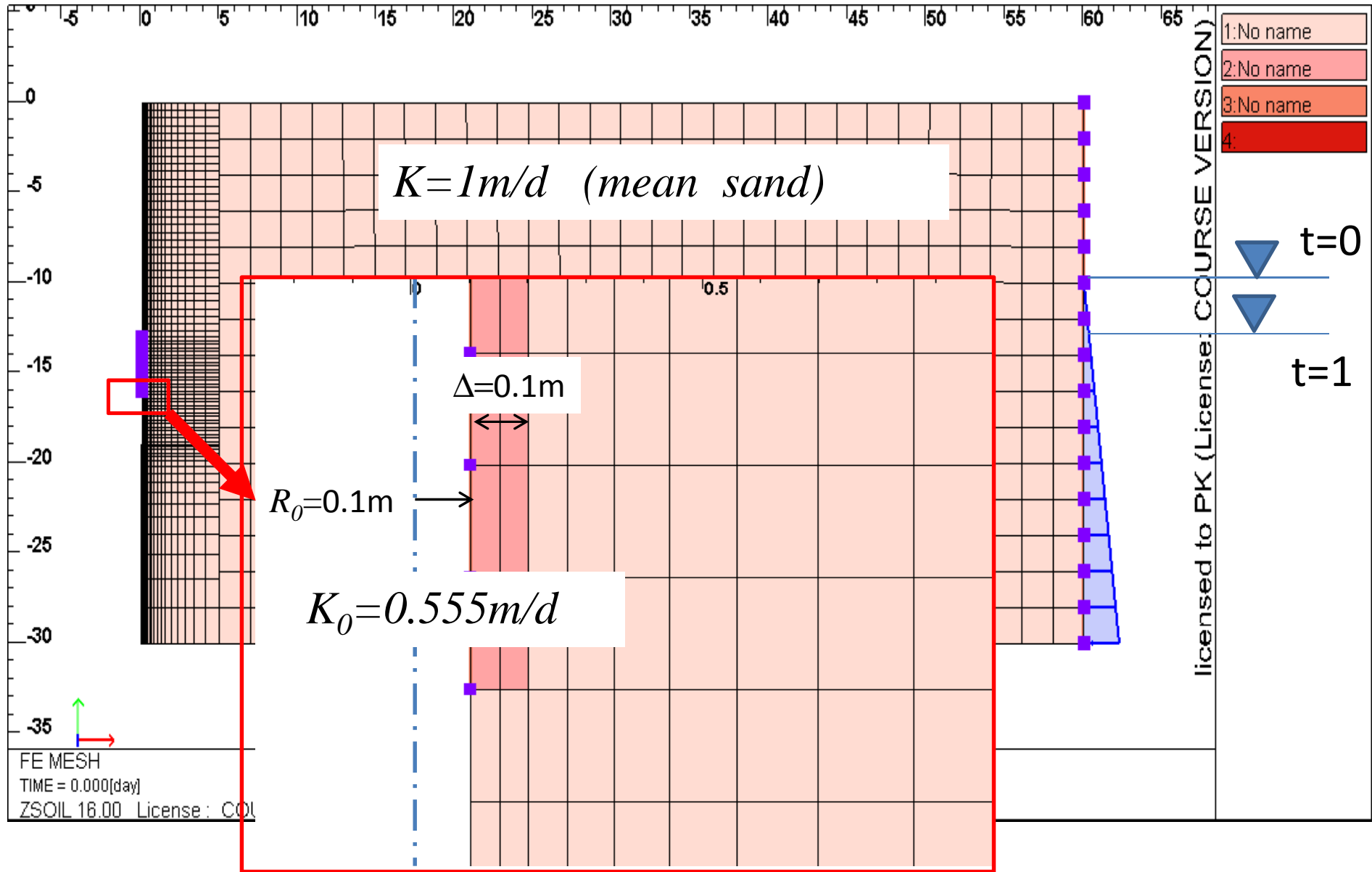
$$R = 1.0, h = 1.0[m] \quad \longrightarrow \quad q = 0.35[m/d]$$

permeability of the layer with assumed thickness  $\Delta = 0.1m$ :

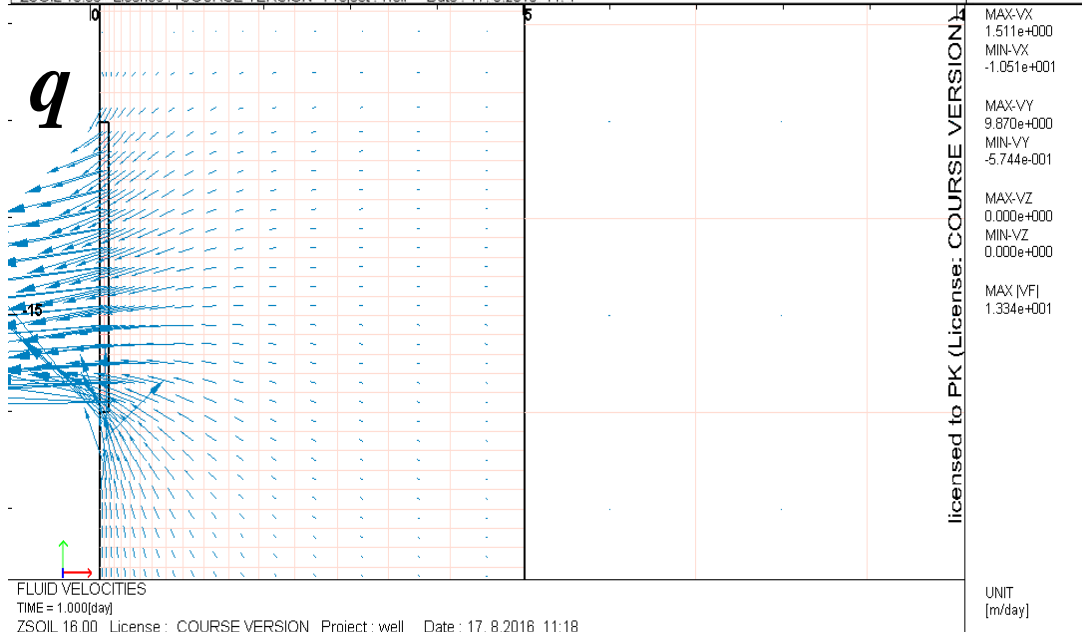
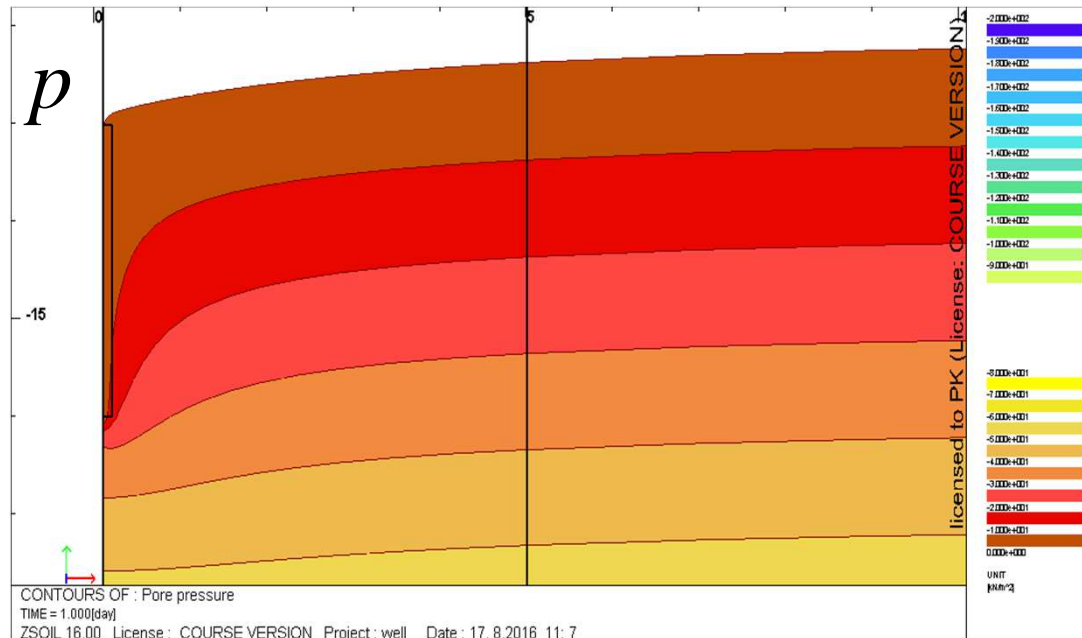
$$\beta = \frac{qR}{Kh} = 0.35 [-]$$

$$K_0 = \frac{0.35 \ln 2}{1 - 0.35 \ln 5} K = \frac{0.35 \cdot 0.693}{1 - 0.35 \cdot 1.609} K = 0.555K$$

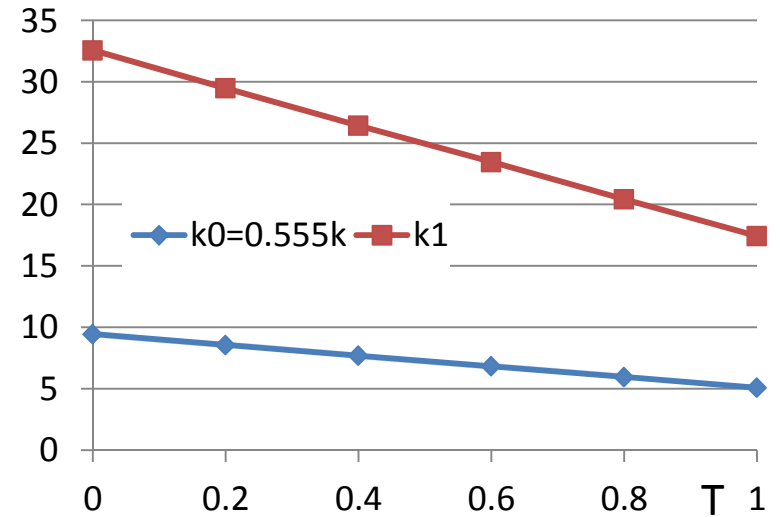
# Axisymmetric macro-model of the well



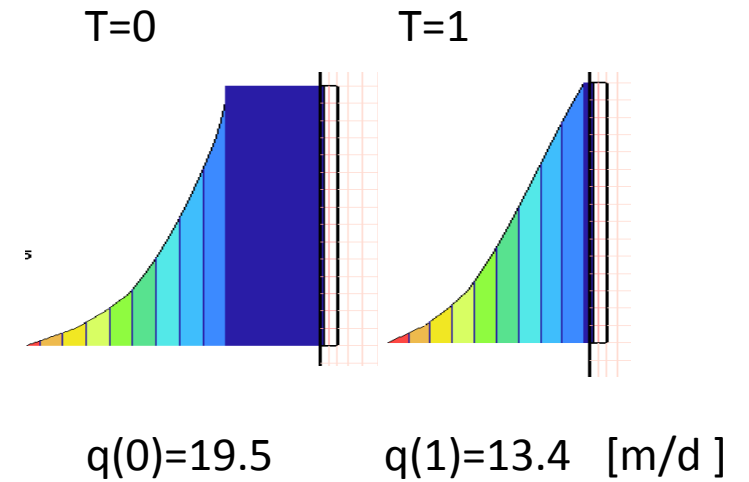
# Results



Outflow Q [m<sup>3</sup>/d]



filtration stream (homogenized)



**Thank you for your attention**

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